

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
28 December 2000 (28.12.2000)

PCT

(10) International Publication Number
WO 00/79648 A1

(51) International Patent Classification⁷: H01Q 15/02, 1/38

(21) International Application Number: PCT/US00/16627

(22) International Filing Date: 16 June 2000 (16.06.2000)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
60/139,712 17 June 1999 (17.06.1999) US

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(81) Designated States (*national*): AE, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CR, CU, CZ, DE, DK, DM, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA, ZW.

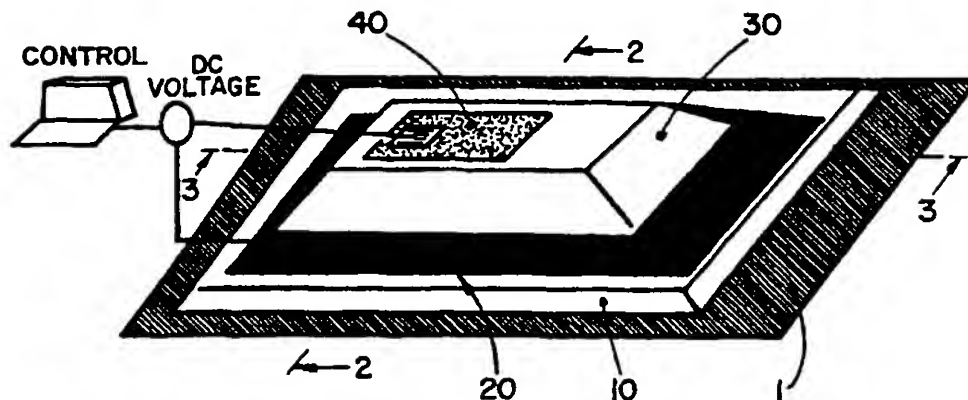
(84) Designated States (*regional*): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).

Published:

— With international search report.

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: TUNABLE DUAL-BAND FERROELECTRIC ANTENNA



(57) Abstract: A multilayer tunable ferroelectric antenna assembly that includes two superimposed substrate layers. A first substrate layer (10) consists of low dielectric material carrying on one face an electrically conductive patch serving as an active feeder-resonator (20). A second substrate (30) includes a ferroelectric material having one face positioned on top of the feeder-resonator (20) and carrying on the opposite face an electrically conductive patch acting as a director (40). The upper director patch is fed through capacitive coupling of energy from the feeder-resonator (20). Application of bias voltage between the director (40) and the feeder-resonator (20) changes the permittivity of the ferroelectric substrate, thereby causing a shift in resonance frequency. A radiation null, corresponding to energy absorption, could be tuned into the resonance frequency at which the antenna is previously exhibiting a radiation characteristic. This provides the antenna a means to behave either as a radiator or an absorber at particular frequency.



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TUNABLE DUAL-BAND FERROELECTRIC ANTENNA

FIELD OF THE INVENTION

This invention relates to a dual band microstrip antenna and, more particularly, to an antenna having a tunable characteristic with the usage of ferroelectric material.

BACKGROUND OF THE INVENTION

There is a considerable demand for antennas that have a dual band performance and a tunable capability for operating in different frequency bands. For example, in wireless communications, the GSM standard used primarily in Europe has frequency bands of 890-915 MHz and 935-960MHz for the uplink and downlink, respectively. In addition to this system, the new generation of personal communication system (PCS), such as DCS 1800, has frequency bands of 1.710-1.785 GHz and 1.805-1.880 GHz for the uplink and downlink, respectively. Hence, for a portable hand-phone to be compatible with the two systems (GSM and PCS) the antenna should be able to operate in these two bands. However, communication standards vary across geographical regions. In North America, the Interim Standard-54 (IS-54) is used instead of the GSM standard. It occupies frequency bands of 869-894 MHz for the uplink and 824-849 MHz for the downlink. The antennas needed for a hand-phone that is useable in both Europe and North America will now be required to cover the three different communication standards.

25

The prior art suggests that this could probably be achieved with multiple antennas or a manual extractable antenna. In most cases, a single plane antenna is preferred. Most of the prior art tunable antennas use diodes or shorting pins to achieve the tuning performance. This additional circuitry adds protrusion and complexity to the antenna structure that limits the capability to operate in a compact, conformal and rugged environment.

30

The use of ferroelectric material in phase shifters is described in "Ceramic Phase Shifters for Electronically Steerable Antenna Systems", Varadan et al., Microwave Journal, January 1992, pages 116-126.

5 Ferroelectric materials have also been described for use in electronic phased scanning periodic arrays. For example such arrays are described in U.S. Patent. No. 5,589,845 to Yandrofski et al., U.S. Patent No. 5,729,239 to Rao and U.S. Patent No. 5,557,286 to Varadan et. al. In such arrays, scanning is achieved by positioning array elements in a linear
10 broadside arrangement. Energy coupling occurs in the horizontal azimuth plane. The common dielectric constant values for Barium Strontium Titanate materials used in the system of the Varadan et al. patent or in the system disclosed in U.S. Patent No. 5,427,988 to Sengupta et al. are relatively high for typical antenna applications.

15

Microstrip antennas with high permittivity substrates have suffered from poor efficiency and narrow bandwidth. The stacking of director elements could enhance the gain and bandwidth and introduce dual band performance. U.S. Patent No 4,162,499 to Jones, Jr. et al. and U.S.
20 Patent No 5,561,435 to Nalbandian et al. suggest stacking of antennas. However, the antennas of these patents are optimized at discrete frequencies only, impeding their use for frequency hopping communication systems.

25 Accordingly, there is a need for a technology and for a single antenna to meet multi-usage and multi-frequency requirements. There is also a need for such antennas to have a planar structure that is flexible enough to conform to hand phone or other wireless device constructions.

30 **SUMMARY OF THE INVENTION**

The present invention provides for an antenna structure that has a dual frequency band performance. Both of the resonant frequency performances are tunable to other frequency bands. For example, the dual

band antenna of our invention can be tuned to the frequency bands of GMS, DCS 1800 and IS-54.

5 The antenna of the present invention has a stacked assembly, in which a first dielectric substrate layer is disposed on top of an electrical ground plane. A feeder radiator is disposed on top of the first dielectric substrate layer. A second substrate layer is disposed on top of the feeder-resonator. The second substrate layer is formed of a tunable ferroelectric material. An electrically conductive director patch is disposed on top of the
10 ferroelectric material.

 In accordance with the invention, the first substrate layer has a permittivity much lower than that of the second ferroelectric substrate layer. It is another feature that the feeder-resonator is designed for a lower
15 frequency operation compared with that of the director. As a result, the feeder-resonator has very large radiating surface area.

 The feeder-resonator serves two purposes: (1) to excite electromagnetic energy for the director element; and (2) to serve as a
20 ground plane for the ferroelectric substrate and the director element. When a DC biasing voltage is applied across the ferroelectric material, the resonant frequencies of the antenna can be tuned or shifted from one frequency range to another based on the value of applied voltage.

25 In accordance with the invention, since the director-radiator is fed through capacitive coupling rather than direct microstrip circuitry, the need for complicated protection circuitry, such as DC blocks, against the high DC bias voltage is eliminated.

30 Another feature of the invention is that a radiation null is tuned in at one of the resonance frequencies, thereby transforming the antenna into an absorber of electromagnetic energy.

BRIEF DESCRIPTION OF THE DRAWING

The objects, advantages and features of the present invention will be understood by reference to the following specification in conjunction
5 with the accompanying drawings, in which like reference characters denote like elements of structure and:

FIG. 1 is a perspective view of the antenna of the present invention.

10 FIG. 2 is a cross sectional view, taken along line 2-2 of FIG. 1.

FIG. 3 is a cross sectional view, taken along the line 3-3 of FIG. 1.

FIG. 4 is a perspective view illustrating a preferred embodiment of
15 the invention.

FIG. 5 is a graph showing the dual-band performance prior to tuning.

20 FIG. 6 is a graph showing the performance of the antenna after tuning with an applied bias voltage across the ferroelectric layer.

DETAILED DESCRIPTION OF THE INVENTION

Referring to FIGS. 1 and 2, the tunable antenna assembly of the
25 present invention includes a first substrate layer 10 having a low loss and low dielectric material available, for example, under the Duroid™ brand from Rogers Corporation of Chandler, Arizona. Disposed on one face of substrate layer 10 is an electrically conductive ground plane 1 and on its opposite face an electrically conductive patch serving as an active feeder-
30 resonator 20. A second substrate 30 has one face positioned on top of feeder-resonator 20 and carrying on its opposite face an electrically conductive patch acting as a director 40. Second substrate 30 is formed of

a ferroelectric material, such as barium strontium titanate or any other low loss perovskite and paraelectric films. The layers of the stacked assembly are adhered to one another by any suitable technique, such as adhesive bonding or microwave joining.

5

First substrate layer 10 has a permittivity value much lower than that of substrate layer 30. Moreover, feeder-resonator 20 is designed for a lower frequency operation compared with director 40. As a result, feeder-resonator 20 has a very large radiating surface area. This allows second
10 substrate layer 30 to be positioned well within the large surface area of feeder-resonator 20.

Feeder-resonator 20 serves the purposes of (1) providing exciting electromagnetic energy for director 40 and (2) serving as a ground plane
15 for ferroelectric substrate layer 30. As shown in FIGS. 1 and 3, a DC biasing voltage 42 is applied across ferroelectric substrate 30, causing a tunable performance on both its resonant frequencies. The stacking structure of ground plane 1, substrate layer 10, feeder radiator 20, second substrate layer 30 and director 40 enhances the gain of resonating director
20 40. A dual-band performance is also achieved through the stacking structure.

Referring to FIG. 4, feeder-resonator 20 is fed by a microstrip circuit 21, while director 40 is fed by capacitive coupling of energy from
25 feeder-resonator 20. This arrangement eliminates the need for complicated protection circuitry, such as DC blocks, against the high DC bias voltage. A DC bias pad 43 is positioned along a centerline of the director 40. A variable voltage source 42, is used to apply a bias voltage between director 40 and feeder-resonator 20, thereby changing the dielectric constant and
30 both resonating frequencies of the antenna.

The dual band performance prior to any applied bias voltages is

illustrated in FIG. 5. A shift in both resonant frequencies due to the applied bias voltage is observed in FIG. 6, verifying the tunability performance obtained with the ferroelectric substrate 30.

5 It has also been observed that a radiation null, corresponding to energy absorption, has been tuned into the upper resonance frequency at which the antenna is previously exhibiting a radiation characteristic. This provides the antenna an ability to behave either as a radiator or an absorber at this particular frequency.

10

The present invention having been thus described with particular reference to the preferred forms thereof, it will be obvious that various changes and modifications may be made therein without departing from the spirit and scope of the present invention as defined in the appended

15 claims.

WHAT IS CLAIMED IS:

1. A tunable dual band antenna comprising:

a stacked assembly that includes:

a layer of ferroelectric material disposed on an electrically conductive feeder-resonator;

an electrically conductive director disposed above said layer of ferroelectric material, wherein electromagnetic energy received by said feeder-resonator is capacitively coupled via said layer of ferroelectric material to said director; and

wherein said stacked assembly exhibits two resonant frequencies that are tunable in response to a bias voltage applied to said layer of ferroelectric material.
2. The tunable dual band antenna of claim 1, wherein said director is disposed on top of said layer of ferroelectric material.
3. The tunable dual band antenna of claim 2, further comprising a ground plane and a layer of dielectric material disposed between said layer of ferroelectric material and said ground plane.
4. The tunable dual band antenna of claim 3, wherein said layer of ferroelectric material has a permittivity value much higher than that of said layer of dielectric material.
5. The tunable dual band antenna of claim 4, wherein said feeder-resonator has a larger surface area compared with that of said second substrate layer of ferroelectric material and that of said director.

6. The tunable dual band antenna of claim 4, wherein said feeder-resonator acts as a ground reference for said layer of ferroelectric material and said director when a DC biasing voltage is applied to said layer of ferroelectric material.

7. The tunable dual band antenna of claim 6, further comprising means for applying said bias voltage across said layer of ferroelectric material to tune said antenna, and wherein said bias voltage is variable.

8. The tunable dual band antenna of claim 7, wherein said bias voltage is variable.

9. The tunable dual band antenna of claim 4, wherein said ferroelectric material includes barium strontium titanate.

10. A method for transforming an antenna into an absorber for electromagnetic energy at a particular frequency comprising the steps of:

providing a layer of ferroelectric material disposed on a feeder-resonator;

providing a director-resonator disposed on top of said layer of ferroelectric material; and

providing a bias voltage across said layer of ferroelectric material.

11. The method of claim 10, further comprising:

providing an electrically conductive ground plane; and

providing a layer of low dielectric material between said layer of ferroelectric material and said ground plane.

12. The method of claim 11, wherein said layer of ferroelectric material has a permittivity value much higher than that of said layer of dielectric material.

13. The method of claim 12, further comprising providing a resistive layer defining a predetermined broken pattern above said director resonator.

14. The method of claim 13, wherein the bias voltage is varied until a radiation null is generated or tuned into a resonance frequency at which the antenna previously exhibited a radiation.

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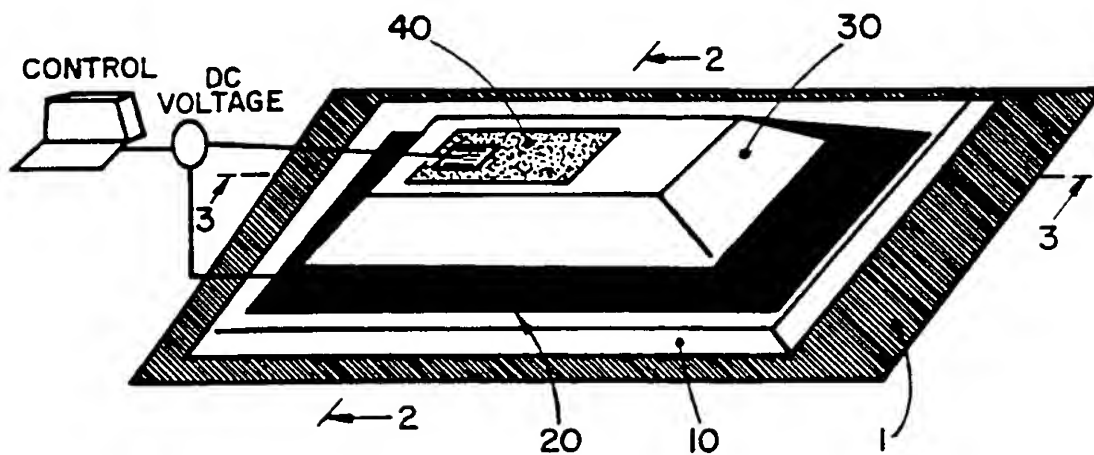


FIG. 1

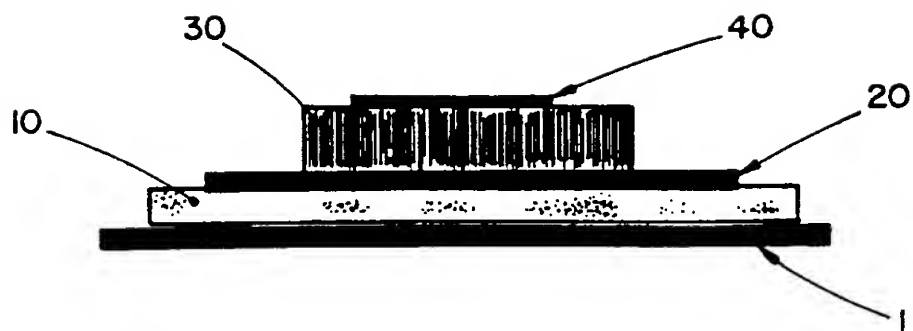


FIG. 2

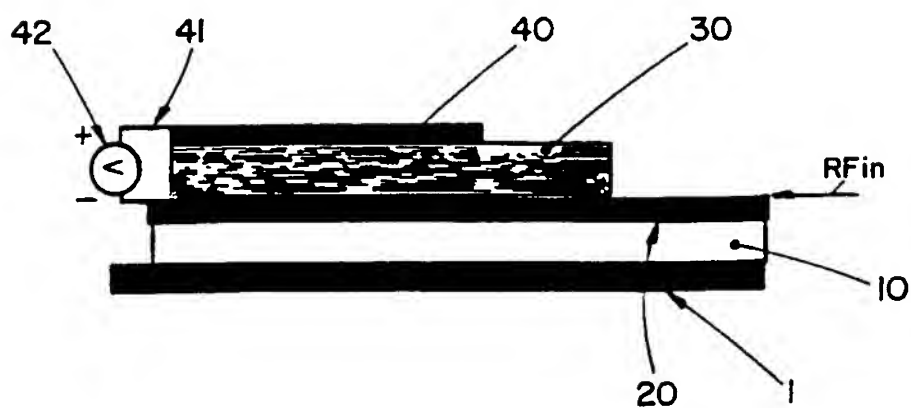


FIG. 3

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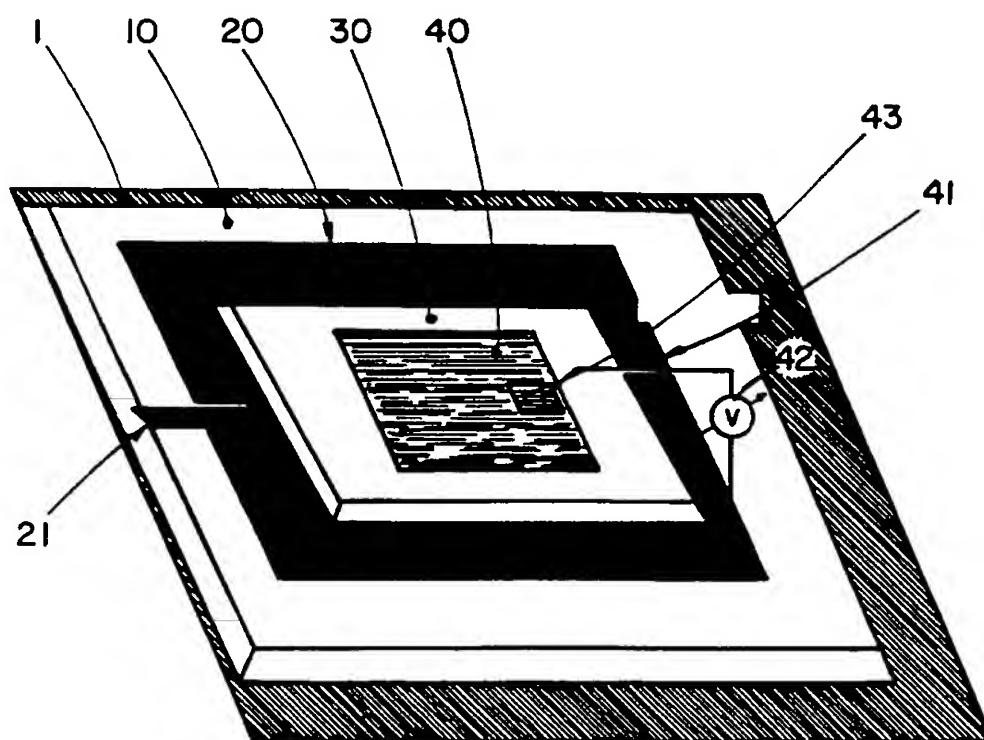


FIG. 4

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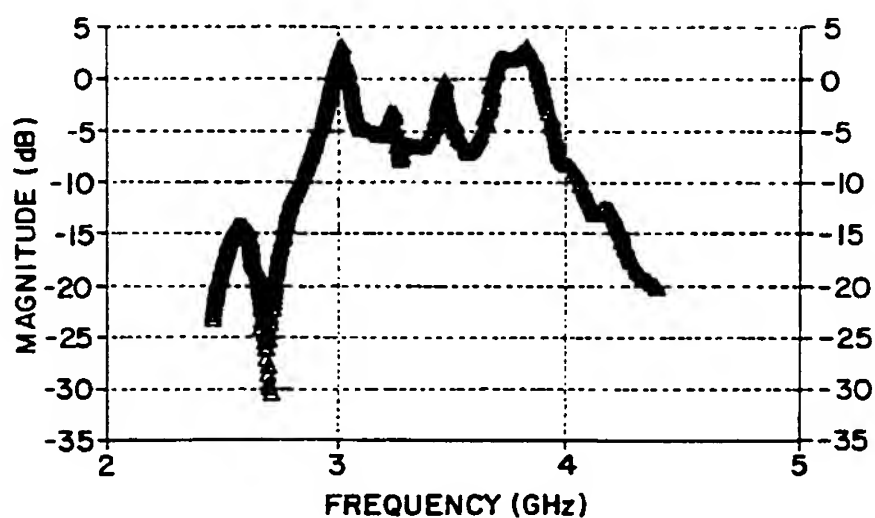


FIG. 5

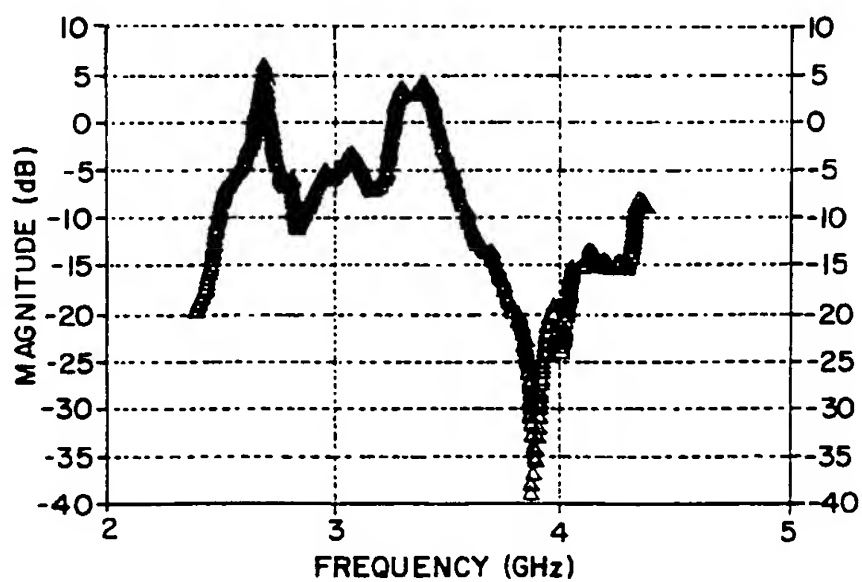


FIG. 6

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US00/16627

A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) H01Q 15/02, 1/38
US CL Please See Extra Sheet.
According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 343/909, 753, 911R; 343/700MS, 853, 909, 753, 911R; 333/161, 995, 24C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5,589,845 A (YANDROFSKI et al) 31 DECEMBER 1996, (31/12/96) entire document.	1-14
Y	US 5,472,935 A (YANDROFSKI et al) 05 DECEMBER 1995, (05/12/95) entire document.	1-14
Y	US 5,617,104 A (DAS) 01 APRIL 1997, (01/04/97) entire document.	1-14
Y	US 5,721,194 A (YANDROFSKI et al) 24 FEBRUARY 1998, (24/02/98) entire document.	1-14
A	US 5,450,092 A (DAS) 12 SEPTEMBER 1995, (12/09/95) entire document.	1-14

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
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L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*G* document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means	
P document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

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Date of mailing of the international search report

11 AUG 2000

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INTERNATIONAL SEARCH REPORT

International application No

PCT/US00/16627

A CLASSIFICATION OF SUBJECT MATTER

US CL

343/909, 753, 911R, 343/700MS, 853, 909, 753, 911R, 333/161, 995